



Blind roll-off estimation for digital transmissions

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ABSTRACT

This paper addresses the problem of estimating the roll-off factor of a received communication signal. We study two new statistical estimation methods that determine the roll-off factor by minimizing the difference between the theoretical and empirical power or power spectral density of the received signal. Another interesting contribution is the derivation of the roll-off Cramér–Rao bound which provides a reference in terms of estimation variance. Simulation results conducted on synthetic data allow the performance of the proposed methods to be evaluated. They are compared to a recent technique based on the amplitude fluctuations of the power spectral density associated with the received communication signal. The estimation methods are shown to be robust to channel impairments (including white Gaussian noise and synchronization errors). The proposed strategies are finally tested on real signals with known ground truth showing their possible application to digital communication problems.

1. Introduction

Linear and nonlinear digital modulation classification has received a lot of attention in the literature. Several classification rules based on the maximum likelihood method [29,9,20,8,11,4,15] or on appropriate features [22,10,24,5,13,21] extracted from the received communication signal have been investigated. The robustness of the resulting classifiers to synchronization errors or channel impairments has also been studied [2,30]. However, in order to classify digital modulations efficiently, the receiver has to know or has to estimate some key parameters associated with the transmitted communication signal. These key parameters include the symbol rate and the shaping filter roll-off factor. Their imperfect knowledge decreases the performance of any digital modulation classifier. Estimating the symbol rate of a communication signal has received much attention in the literature. For instance, several symbol rate estimators take advantage of the cyclostationarity of communication signals [6,12]. This paper focuses on the roll-off estimation problem for classical transmission systems which are based on linear modulations relying on square root raised cosine (SRRC) shaping. To our knowledge, the only available roll-off estimation method is based on the waveform of the received signal [26]. This may be explained by the negligible impact of roll-off mismatched factors on the BER (see [18] or [27]). However, the performance of a digital modulation classifier is affected by a roll-off estimation error. Indeed, a roll-off error induces some noise enhancement (ISI introduced because the Nyquist criterion is no longer

fulfilled) and some reduction in the power of the useful signal (absence of matched filtering). This impact is particularly significant for new high order constellations. Fig. 1 shows an example of a possible high order transmitted constellation (32-APSK, in DVB-S2 standard [1]). Fig. 2 shows how this constellation can be disturbed when the receiver roll-off factor is different compared to the transmitter's one (transmitter roll-off = 0.7, receiver roll-off = 0.2), especially in the presence of other impairments such as noise or errors on the carrier frequency. The ISI due to the fact that the Nyquist criterion is no longer fulfilled and the reduction in SNR due to the absence of matched filtering lead to increase the degradations in the received signal and further disturb the digital modulation classification process.

Another advantage of estimating accurately the roll-off factor is spectrum supervision. In that case, it permits to check whether the transmitter uses an authorized roll-off or not. As an example, Thales Alenia Space offers end-to-end solutions for satellite frequency monitoring and interception, for satellite operators, national regulatory or defence agencies. In these solutions, the carrier detection and characterization relies on the Thales product referred to as telecom carrier analyzer (TCA). The TCA provides a large number of features, such as RF parameters (power, bandwidth, etc), digital characterization (modulation, symbol rate, inner and outer codes, etc.), from blind carrier detection to inside carrier characterization. Roll-off estimation is an interesting parameter that could be added to this list, allowing better classification performance to be obtained. Moreover, this parameter is directly related to the occupied bandwidth of the received communica-

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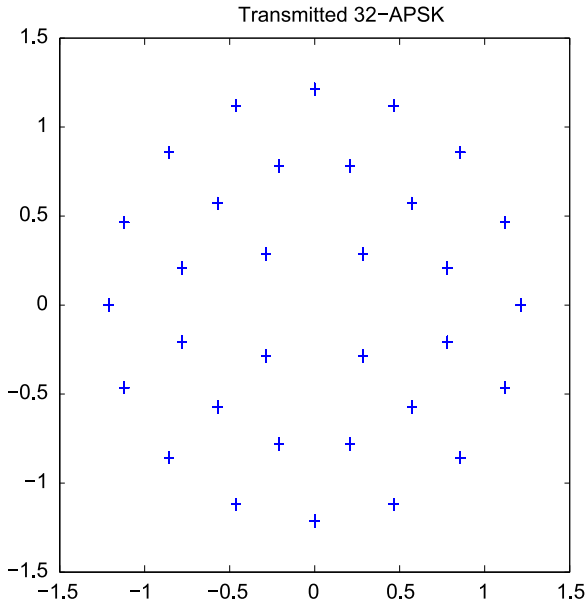


Fig. 1. Transmitted 32-APSK constellation.

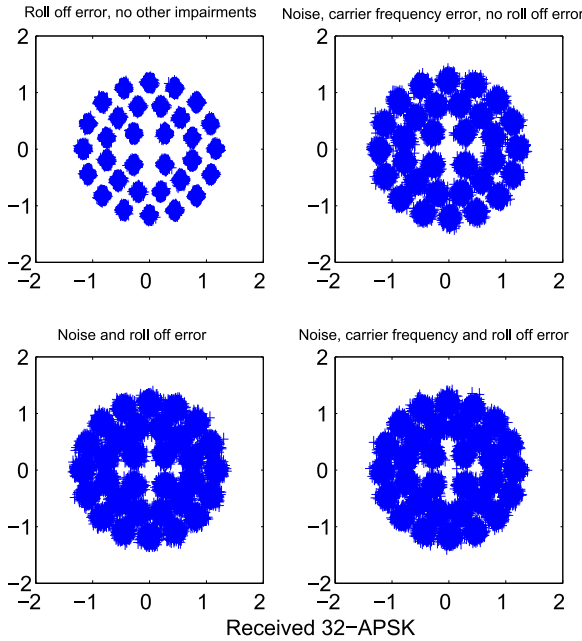


Fig. 2. Received 32-APSK constellations.

tion signal, which allows this bandwidth to be estimated, which is important in non-cooperative scenarios. Indeed, to increase their bit error rates some transmitters can use more than the authorized bandwidth by modifying the roll-off factor, generating some cross-talk. Estimating the spectral bandwidth accurately is a way of identifying these transmitters, which requires to estimate the symbol rate and the roll-off factor of the received communication signal.

This paper studies two new roll-off estimation methods that have some clear advantages with respect to the method studied in [26], which will be used as a benchmark for our study. It is organized as follows. Section 2 presents a model of the received baseband communication signal including some practical channel impairments. Section 3 analyzes the impact of a roll-off mismatch on the BER. Section 4 studies the first proposed estimation method based on the power spectral density (PSD) of the received signal. Section 4 also introduces a second method based on the power of the received communication

signal. Section 5 derives the modified Cramer Rao bound (MCRB) [7] for the roll-off estimation problem. The MCRB provides a reference in terms of mean square error (MSE) for any unbiased estimator of a given parameter. It is used here to evaluate the optimal performance of roll-off estimators. Simulation results presented in Section 6 allow one to appreciate the performance of the proposed methods with respect to [26]. The robustness of the proposed algorithms to carrier phase and frequency errors is also investigated. Simulations performed on real satellite signal measurements (provided by Thales Alenia Space) finally show the applicability of the proposed methods to real scenarios. Conclusions and future works are reported in Section 7.

2. Signal model

Consider an additive white Gaussian noise (AWGN) channel resulting from the forward link of a fixed broadband satellite system. The complex envelope $r(t)$ associated with a received communication signal can be written as

$$r(t) = s(t) + n(t)$$

where $n(t)$ is the complex envelope (or equivalent low-pass signal) of the incoming noise of power spectral density $N_0/2$ and $s(t)$ denotes the complex envelope of the incoming communication signal. In the presence of synchronization impairments, $s(t)$ can be written as

$$s(t) = \sum_k d_k h(t - kT_s - \tau) e^{j(2\pi\Delta f t + \phi)} \quad (1)$$

where

- $\{d_k\}$ is the complex data symbol sequence (supposed to be zero mean, independent and identically distributed (i.i.d.)),
- $h(t)$ is the impulse response of the emission filter,
- T_s is the symbol duration, ϕ
- and Δf are the carrier phase and the carrier frequency errors, τ
- denotes the clock phase error.

A communication system based on linear modulations relying on square root raised cosine (SRRC) shaping is considered in this paper. The resulting shaping filter impulse response is defined as

$$h(t) = 4\alpha \frac{\cos[(1 + \alpha)\pi R_s t] + \frac{\sin[(1 - \alpha)\pi R_s t]}{4\alpha R_s}}{\pi [1 - (4\alpha R_s)^2] / \sqrt{R_s}} \quad (2)$$

where α represents the roll-off parameter defining the shaping filter and $R_s = 1/T_s$ is the symbol rate. As mentioned before, in order to simultaneously avoid interference between the transmitted symbols and minimize the bit error rate, the same SRRC filters have to be used at the transmitter and at the receiver. Consequently, the receiver has to know *a priori* the roll-off parameter α of the SRRC filter. When this knowledge is not available, this parameter can be estimated from the received communication signal $r(t)$. Before addressing this estimation problem, the next section studies the impact of a roll-off mismatch on the transmission.

3. Impact of a roll-off mismatch on the bit error rate

This section first recalls the theoretical expression of the BER for a Gaussian channel, without synchronization errors (i.e., $\phi = \Delta f = \tau = 0$) with the same SRRC filters at the transmitter and the receiver. The impact of a roll-off mismatch between the transmitter and the receiver on the BER is then analyzed.

3.1. BER for an ideal AWGN channel

When the transmitter and receiver filters have the same roll-off factor, the Nyquist criterion ensuring interference free transmission is

fulfilled. As a consequence, the received symbols after matched filtering and sampling is [19]

$$\tilde{d}_m = d_m g(t_0) + w_m \quad (3)$$

where

- the sampling instants $t_0 + mT_s$ are chosen in order to avoid inter symbol interference (ISI),
- $g(t) = h(t) * h_r(t)$ is the impulse response of the global transmission channel, where $h(t)$ and $h_r(t)$ are the impulse responses of the filters associated with the transmitter and the receiver
- w_m is a complex Gaussian noise with variance $2\sigma^2$ (σ^2 denotes the variance of the real and imaginary complex noise components).

The expression of the BER is well known in this scenario. For example, considering a squared M -QAM modulation

$$d_k = a_k + jb_k, \quad a_k, b_k \in \{\pm V, \pm 3V, \dots, \pm \sqrt{M}V\}$$

the symbol error rate (SER) is given by [19]

$$\text{SER} = 4 \left(1 - \frac{1}{\sqrt{M}}\right) Q \left[\sqrt{\frac{g(t_0)}{\sigma}} \right] \quad (4)$$

where $Q(\cdot)$ denotes the complementary cumulative distribution function (CCDF) of a standard Gaussian random variable. When the filter used by the receiver is identical to the filter used by the transmitter, the following results can be obtained

$$\sigma^2 = N_0 \int_{-\infty}^{\infty} |H_r(f)|^2 df = N_0 g(t_0) = N_0, \quad (5)$$

where $H_r(f)$ is the receiver filter transfer function. Note that

$$E_s = E_b \log_2(M) = \frac{\sigma_d^2}{2} \int_{-\infty}^{\infty} |H(f)|^2 df = \frac{\sigma_d^2}{2} g(t_0) = \frac{\sigma_d^2}{2}$$

where E_s and E_b are the averaged symbol and bit energies, and σ_d^2 is the symbol variance. When using a Gray mapping, this leads to the following classical BER expression:

$$\text{BER} \approx \frac{4}{\log_2(M)} \left(1 - \frac{1}{\sqrt{M}}\right) Q \left(\sqrt{\frac{3 \log_2(M) E_b}{M-1 N_0}} \right). \quad (6)$$

3.2. Impact of a roll-off mismatch

When the transmitter and receiver filters do not have the same roll-off factor, (3) has to be replaced by

$$\tilde{d}_m = d_m g(t_0) + \sum_{k \neq m} d_k g[t_0 + (k-m)T_s] + w_m \quad (7)$$

where $\sum_{k \neq m} d_k g[t_0 + (k-m)T_s]$ is an interference term that has not been canceled because the transmission channel no longer satisfies the Nyquist criterion. It is interesting to note that the BER associated with (7) has increased when compared to the BER resulting from (3) because of ISI.

When the number of samples in the right hand side of (7) is sufficiently large, the central limit theorem can be used to assume that

$$\sum_{k \neq m} d_k g[t_0 + (k-m)T_s] \quad (8)$$

is an additional complex Gaussian noise with variance $2\sigma_{\text{ISI}}^2$, σ_{ISI}^2 denoting the variance of the real and imaginary complex ISI components. The BER degradation due to roll-off mismatch can then be quantified by evaluating the variance of the additional term (8) due to ISI. For instance, considering squared M -QAM modulations, the SER can be expressed as follows:

$$\text{SER} = 4 \left(1 - \frac{1}{\sqrt{M}}\right) Q \left(\sqrt{\frac{g(t_0)}{\sigma_a}} \right) \quad (9)$$

with $\sigma_a^2 = \sigma^2 + \sigma_{\text{ISI}}^2$. Due to roll-off mismatch (or equivalently to unmatched filtering), the following result is obtained ($g(t_0) \neq 1$ here)

$$\text{BER} \approx \frac{4 \left(1 - \frac{1}{\sqrt{M}}\right)}{\log_2(M)} Q \left(\sqrt{\frac{3 \log_2(M) E_b}{M-1 N_0} \frac{g(t_0)}{1 + \frac{\sigma_{\text{ISI}}^2}{N_0}}} \right). \quad (10)$$

Comparing expressions (10) and (16), the degradation on the BER (expressed in decibels) due to the roll-off error can be written as

$$D(\text{dB}) = 10 \log_{10} \left(\frac{g(t_0)}{\sqrt{1 + \frac{\sigma_{\text{ISI}}^2}{N_0}}} \right) \quad (11)$$

where σ_{ISI}^2 can be easily computed for independent symbols as follows

$$\sigma_{\text{ISI}}^2 = \frac{\sigma_d^2}{2} \sum_{k \neq m} g^2[t_0 + (k-m)T_s]. \quad (12)$$

4. Roll-off estimation

The previous section has analyzed the impact of a roll-off mismatch on the performance of a communication system. This section studies different roll-off estimation methods. The accurate knowledge of the roll-off factor allows the effect of the ISI term (outlined in the previous section) to be mitigated, but can also be used to improve the signal bandwidth estimation. Indeed, bandwidth estimation, which is an important parameter for spectrum supervision, is currently achieved by estimating the symbol rate R_s and by using the following estimator

$$\hat{B} = (1 + \alpha_e) \hat{R}_s$$

which assumes that the roll-off of the emission filter, α_e , is known. In practical estimations where the parameter α_e is unknown, it is interesting to design roll-off estimation methods. This problem has received few attention in the literature. A spectral technique was investigated in [26], based on the PSD of the received communication signal. The inverse fast Fourier transform of this PSD has a raised cosine pulse shape whose amplitude fluctuations are related to the roll-off factor. The authors of [26] proposed to use the ratio between the main and first secondary lobe amplitudes of this raised cosine shape for roll-off estimation. However, we have observed that this method suffers from noise and other channel impairments like synchronization errors. This section introduces two new roll-off estimation methods based on the spectrum and the power of the received communication signal. These methods are then compared with the method of [26] in Section 6 (in terms of performance and robustness to synchronization errors).

4.1. Estimation method based on the received signal PSD

If the transmitted signal shaping is an SRRC, the roll-off parameter of the emission filter can be estimated by minimizing the distance between the estimated PSD of the complex envelope of $r(t)$ denoted as $S_r(f)$ and its theoretical expression $S(f, \alpha_e)$, i.e.,

$$\hat{\alpha}_{\text{PSD}} = \arg \min_{\alpha_e} \int_{-\infty}^{\infty} [S_r(f) - S(f, \alpha_e)]^2 df. \quad (13)$$

This method differs from the one proposed in [26] by the fact that the spectrum is directly used instead of the amplitudes of the two main

time response raised cosine lobes. For a zero mean i.i.d. complex symbol sequence and AWGN channel, the PSD of the received communication signal complex envelope is known to be [19]

$$S(f, \alpha_e) = \frac{\sigma_d^2}{T_s} |H(f)|^2 + 2N_0 \quad (14)$$

where

$$|H(f)|^2 = \begin{cases} T_s & \text{if } |f| \leq \frac{1-\alpha_e}{2T_s} \\ \frac{T_s}{2} \left[1 + \sin \frac{\pi T_s}{\alpha_e} \left(\frac{1}{2T_s} - |f| \right) \right] & \text{if } \frac{1-\alpha_e}{2T_s} \leq |f| \leq \frac{1+\alpha_e}{2T_s} \\ 0 & \text{elsewhere} \end{cases} \quad (15)$$

when using an SRRC pulse shaping. Note that the PSD $S_r(f)$ will be estimated using a Welch periodogram [23], that N_0 is assumed to be known and that the optimization method used to solve (13) is the Nelder–Mead (NM) method [14]. The NM method is a simplex method whose efficiency has been proved in many applications. The main idea is to build a sequence of simplices (polytopes of $n+1$ vertices in n dimensions) by simple operations such as reflections, expansions, contractions or shrinks in order to approximate the minimum of the objective function (see [16] for more details). Table 1 presents the time it takes to classify a modulation for different numbers N_s of samples. This classification does not need to be made in real time. However, the decision has to be taken as fast as possible, which is satisfactory for $N_s=10,000$ observed symbols.

4.2. Estimation based on the received signal power

The method considered in this section filters the received communication signal by an SRRC filter. If the roll-off parameter of this filter matches the roll-off of the transmitter, the received symbols after matched filtering and sampling can be written as in (3) and no longer as in (7). The interference term is canceled (due to the fact that the Nyquist criterion is fulfilled, see [25, pp. 556–557]) and the power of the useful term is maximized (due to matched filtering, see [25, pp. 236–242]). This section studies a roll-off estimator taking advantage of this property. More precisely, using (7), the power of the received signal filtered by an SRRC filter with roll-off factor α_r and sampled at $t_0 + mT_s$ is

$$P(\alpha_r | t_0, \sigma^2) = E[|\tilde{d}_m|^2] = \sigma_d^2 g^2(t_0) + 2\sigma_{\text{ISI}}^2 + 2\sigma^2 \quad (16)$$

where the interference and useful terms depend on α_r through the expression of the impulse response $g(t)$. Fig. 3 displays a typical evolution of the power $P(\alpha_r | t_0, \sigma^2)$ as a function of α_r for a given value of the transmitter roll-off $\alpha_e = 0.35$. This figure shows that the power at the output of the receiver SRRC filter is maximum (due to matched filtering) for $\alpha_r = \alpha_e$.

Based on (16), an estimator of α_e can be defined as follows

$$\hat{\alpha}_p = \arg \max_{\alpha_r} P(\alpha_r | t_0, \sigma^2) \quad (17)$$

provided that t_0 is known. The absence of knowledge about t_0 can be alleviated by using the following roll-off estimation procedure.

1. Sample the received signal at rate $2R_s$ in order to fulfill the sampling

Table 1
Computation time versus number of observed symbols.

N_s	Computation time (ms)
500	52.64
1000	28.82
2000	57.79
5000	88.29
10,000	167.92

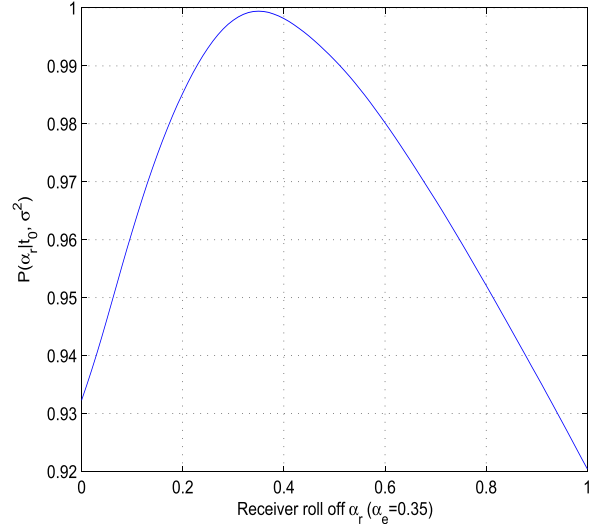


Fig. 3. $P(\alpha_r | t_0, \sigma^2)$ as a function of α_r for $\alpha_e = 0.35$.

Nyquist criterion. Note that there are several techniques that can be used for the blind estimation of the symbol rate. The method proposed in [12] has been considered here for its simplicity.

2. Estimate the optimal sampling instants using the method described in [17], leading to $\hat{t}_0$.
3. Estimate α_e by maximizing (16) after replacing t_0 by its estimator, i.e.,

$$\hat{\alpha}_p = \arg \max_{\alpha_r} P(\alpha_r | \hat{t}_0, \sigma^2). \quad (18)$$

Again, the optimization method used to solve (18) is the Nelder–Mead method.

5. Cramer–Rao Bound for the roll-off estimation problem

In order to obtain a reference in terms of estimation variance, it is usual to determine the Cramer–Rao bound associated with the parameters to be estimated. This section derives bounds for the estimation of the roll-off factor α_e . As explained before, in the presence of synchronization errors, the received signal depends on the roll-off factor but also on parameters related to synchronization impairments (classically referred to as unwanted or nuisance parameters). These parameters include the clock phase error τ and the residual carrier frequency and phase Δf and ϕ . Because of the presence of nuisance parameters and also because the complex data symbols belong to a finite alphabet, the exact Cramer–Rao bound associated with the parameters contained in the received communication signal cannot be computed in closed form. A classical way of solving this problem is to consider the following modified Cramer–Rao bound (MCRB) [7]

$$\text{MCRB}(\alpha) = \frac{1}{E_{r,u} \left\{ \left[\frac{\partial \ln p(\mathbf{r} | \mathbf{u}, \alpha)}{\partial \alpha} \right]^2 \right\}} \quad (19)$$

where $\mathbf{r} = [r(1), \dots, r(N)]^T$ is the finite-dimensional observed vector and $\mathbf{u}$ is a vector containing the nuisance parameters τ , Δf , ϕ and the data symbols d_k . It is shown in [25] that in the limit, as the number of dimensions of $\mathbf{r}$ tends to infinity, the MCRB (19) can be computed by replacing $p(\mathbf{r} | \mathbf{u}, \alpha)$ by the following continuous-time function

$$\Lambda(\alpha, \mathbf{u}) = \exp \left[-\frac{1}{N_0} \int_{T_0} s(t) r(t) dt - \frac{1}{2N_0} \int_{T_0} |s(t)|^2 dt \right] \quad (20)$$

where T_0 denotes the observation interval. Straightforward computations finally lead to the following result:

$$\text{MCRB}(\alpha) = \frac{N_0}{E_u \left[\int_{T_0} \left| \frac{\partial s(t)}{\partial \alpha} \right|^2 dt \right]}. \quad (21)$$

Using (1), we obtain

$$\int_{T_0} \left| \frac{\partial s(t)}{\partial \alpha} \right|^2 dt = \sum_{k,m} d_k d_m^* \int_{T_0} q_\alpha(t - kT_s - \tau) q_\alpha(t - mT_s - \tau) dt \quad (22)$$

where $q_\alpha(t) = \frac{\partial h(t)}{\partial \alpha}$. As indicated in (21), the statistical expectation of (22) with respect to the data symbols d_k and the nuisance parameters τ , Δf , ϕ needs to be computed. The computations are very similar to the ones related to the estimation of the carrier frequency, carrier phase and timing epoch derived in [7]. The next result follows from (22) by recalling that symbols $\{d_k\}$ are assumed to be i.i.d. with zero mean and variance σ_d^2

$$E_d \left[\int_{T_0} \left| \frac{\partial s(t)}{\partial \alpha} \right|^2 dt \right] = \sigma_d^2 \int_{T_0} \sum_k q_\alpha^2(t - kT_s - \tau) dt. \quad (23)$$

The Poisson formula [3] leads to

$$\sum_k q_\alpha^2(t - kT_s - \tau) = \frac{1}{T_s} \sum_k Q_{2,\alpha} \left(\frac{k}{T_s} \right) e^{j2\pi k \left(\frac{t-\tau}{T_s} \right)} \quad (24)$$

where $Q_{2,\alpha}(f)$ is the Fourier Transform of $q_\alpha^2(t)$. After substituting (24) in (23) and averaging with respect to τ (considered as a discrete random variable uniformly distributed between 0 and T_s)

$$\begin{aligned} E_u \left[\int_{T_0} \left| \frac{\partial s(t)}{\partial \alpha} \right|^2 dt \right] &= E_\tau \left[E_d \left[\int_{T_0} \left| \frac{\partial s(t)}{\partial \alpha} \right|^2 dt \middle| \tau \right] \right] \\ &= \frac{1}{T_s} \int_0^{T_s} \sigma_d^2 \int_{T_0} \frac{1}{T_s} \sum_k Q_{2,\alpha} \left(\frac{k}{T_s} \right) e^{j2\pi k \left(\frac{t-\tau}{T_s} \right)} dt d\tau \\ &= \frac{\sigma_d^2 T_0}{T_s} \sum_k Q_{2,\alpha} \left(\frac{k}{T_s} \right) \text{sinc} \left(\frac{\pi k T_0}{T_s} \right) \text{sinc}(\pi k) e^{j\pi k \left(\frac{T_0}{T_s} - 1 \right)} \end{aligned} \quad (25)$$

where $\text{sinc}(x) = \frac{\sin(x)}{x}$. Straightforward computations finally lead to

$$E_u \left[\int_{T_0} \left| \frac{\partial s(t)}{\partial \alpha} \right|^2 dt \right] = \frac{\sigma_d^2 T_0}{T_s} Q_{2,\alpha}(0) \quad (26)$$

with

$$Q_{2,\alpha}(0) = [Q_\alpha(f) \otimes Q_\alpha(f)]_{f=0} \quad (27)$$

where $\otimes$ denotes convolution and $Q_\alpha(f)$ is the Fourier transform of $q_\alpha(t)$. Using the property that $Q_\alpha(f)$ is an Hermitian function (since $q_\alpha(t)$ is a real function), the following result can be obtained

$$Q_{2,\alpha}(0) = \int_{-\infty}^{\infty} |Q_\alpha(u)|^2 du = \int_{-\infty}^{\infty} |q_\alpha(u)|^2 du. \quad (28)$$

By denoting as N_s the number of symbols in the observation interval T_0 , (26) and (28) lead to

$$\text{MCRB}(\alpha) = \frac{N_0}{\sigma_d^2 N_s P_\alpha} \quad (29)$$

where $N_s = \frac{T_0}{T_s}$ and $P_\alpha = \int_{-\infty}^{\infty} |Q_\alpha(u)|^2 du = \int_{-\infty}^{\infty} |q_\alpha(u)|^2 du$. Denoting the symbol energy as

$$E_s = E_b \log_2(M) = \frac{\sigma_d^2}{2} \int_{-\infty}^{\infty} |H(f)|^2 df = \frac{\sigma_d^2}{2}$$

and using symbolic computations leading to $P_\alpha = \frac{\pi^2}{48\alpha}$, the following expression is finally obtained

$$\text{MCRB}(\alpha) = \frac{24\alpha}{\pi^2 \frac{E_b}{N_0} \log_2(M) N_s}. \quad (30)$$

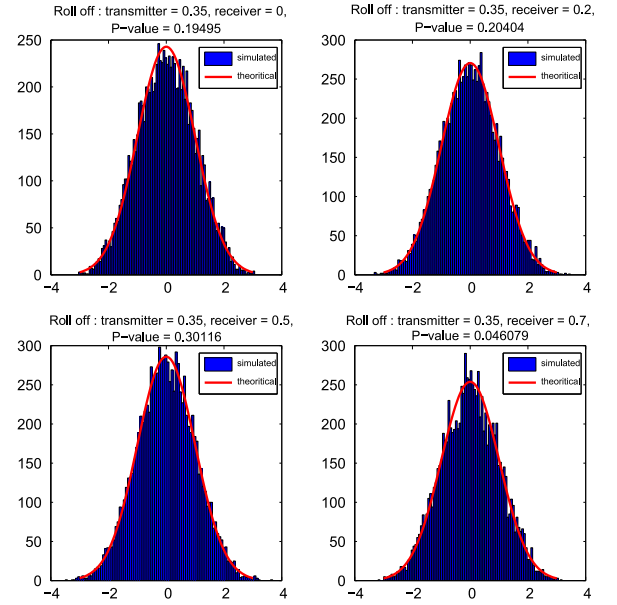


Fig. 4. Estimated and fitted Gaussian pdfs for the interference term to the roll-off mismatch.

6. Simulation results

6.1. Impact of a roll-off mismatch

Even if the number of samples in (8) depends on the roll-off factor (this number increases as the roll-off factor decreases), Fig. 4 shows qualitatively that the Gaussian assumption for the additional term due to roll-off mismatch is valid for all roll-off factors. Quantitative results coming from the application of the Kolmogorov test confirm the validity of the Gaussian assumption for (8) since the P -values indicated on each figure are clearly in favor of accepting the Gaussian assumption with usual probabilities of false alarm (see Fig. 4). Fig. 5 illustrates this property, showing received QPSK constellations (plotted after filtering) with and without roll-off impairment. The top figure has been obtained with identical filters at the emitter and the receiver (without additive noise). The middle figure corresponds to a roll-off mismatch (roll-off at the emitter side $\alpha_e = 0.35$, roll-off at the receiver side $\alpha_r = 0.7$) which clearly shows the additional noise affecting the QPSK constellation. The bottom figure has been obtained with identical emitter and receiver filters (i.e., $h_r(t) = h(t)$) with an additive Gaussian noise whose variance

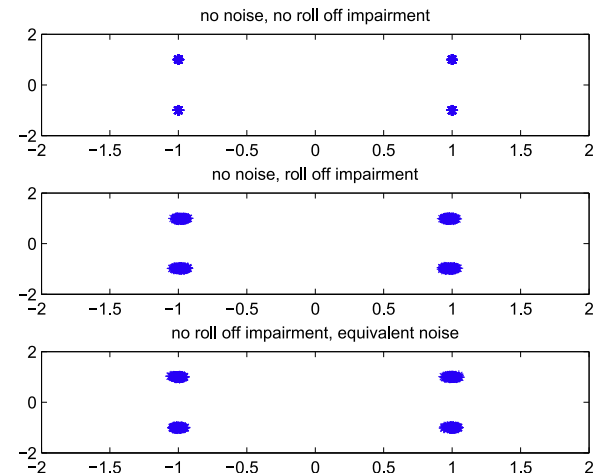


Fig. 5. QPSK constellations with and without roll-off impairment.

has been set to the variance of the constellation obtained with the previous roll-off mismatch. These results confirm that the ISI term due to the roll-off impairment can be approximated by an additional Gaussian noise with good accuracy.

Denoting as α_e and α_r the roll-off factors of the transmission and reception filters, Fig. 6 compares the BERs obtained for $\alpha_e = \alpha_r = 0.5$ (no roll-off error) and for $\alpha_e = 0.5$, $\alpha_r = 0.2$ (roll-off error) using the theoretical expression (10) and an estimation computed from 10^5 emitted symbols. The BERs are displayed as a function of E_b/N_0 for a 4-QAM (or QPSK) modulated signal. It can be noted that there is a good match between the theoretical and experimental BERs, validating the assumption that the interference term can be approximated by an additive Gaussian noise. Fig. 7 shows the corresponding degradation as a function of α_r for $\alpha_e = 0.5$ and for different values of E_b/N_0 . As expected, for low roll-off values the degradation due to a roll-off mismatch is higher due to more powerful side lobes of $g(t)$ yielding more powerful interference terms (as shown in Fig. 8).

6.2. Performance of the roll-off estimation methods

The objective of this section is to compare the performance of different roll-off estimation methods. More precisely, we consider the spectral method of [26] (referred to as “Xu”) and the two proposed strategies based on the power and PSD of the received communication signal (referred to as “Power” and “PSD” respectively). Table 2 summarizes the simulation parameters used for the comparison.

Fig. 9(a) shows the estimated MSEs as a function of the number of

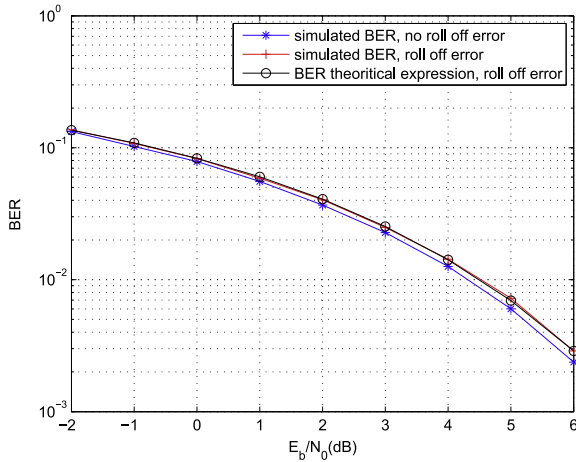


Fig. 6. Theoretical and simulated BER obtained with and without roll-off errors.

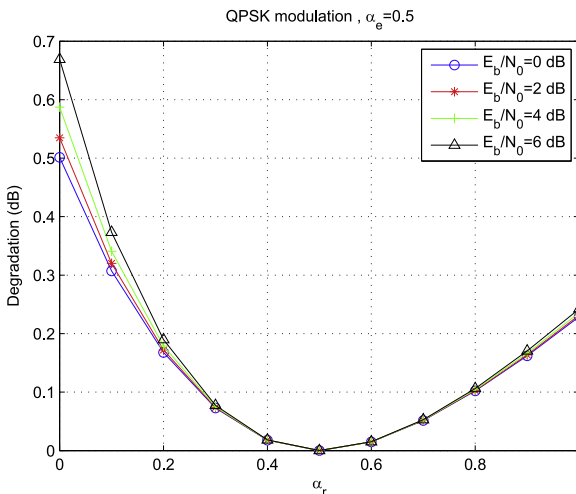


Fig. 7. BER degradation as a function of α_r for $\alpha_e = 0.5$ and several values of E_b/N_0 .

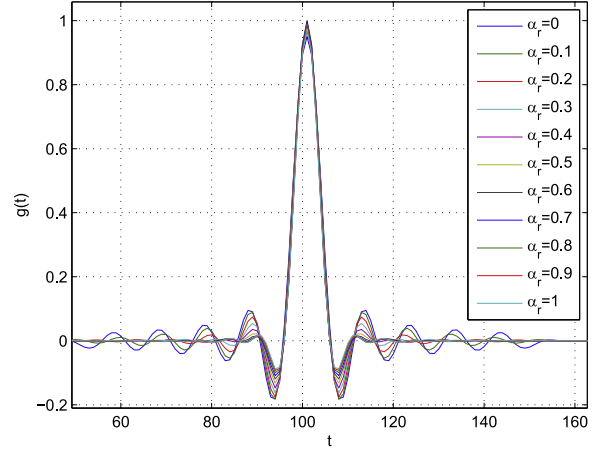


Fig. 8. Channel impulse response $g(t)$ for several values of α_r , $\alpha_e = 0.5$.

Table 2
Simulation parameters.

Considered modulations	QPSK, 8-PSK, 16-QAM
Shaping filter	Square root raised cosine
Roll-off	$\alpha_e = 0.2$ (DVB-S2[1])
Filter length	$20T_s$
Number of Monte Carlo runs	10,000

observed symbols N_s in absence of noise, whereas Fig. 9(b) corresponds to $E_b/N_0 = 0$ dB. The algorithm based on the power of the received signal has clearly the best performance. The performances of the roll-off estimation methods are depicted in Fig. 10. The MSEs of the roll-off estimates are clearly decreasing when the number of samples N_s is increasing or when E_b/N_0 is increasing, as expected.

Fig. 11 compares the performance of the power-based strategy for different modulations and $E_b/N_0 = 0$ dB. It appears that the power-based roll-off estimation method performs better for high efficiency modulations. This is due to the fact that the SNR increases with the modulation order M . Indeed, this SNR can be expressed as

$$\text{SNR} = [(\text{SNR}_w)^{-1} + (\text{SNR}_{\text{ISI}})^{-1}]^{-1} \quad (31)$$

where SNR_{ISI} (which does not depend on M) is the SNR related to the ISI part of (7) defined as

$$\text{SNR}_{\text{ISI}} = \frac{\sigma_d^2 g^2(t_0)}{2\sigma_{\text{ISI}}^2} = \frac{g^2(t_0)}{\sum_{k \neq m} g^2[t_0 + (k - m)T_s]} \quad (32)$$

and SNR_w is the required SNR, i. e., the SNR related to the noise in (7)

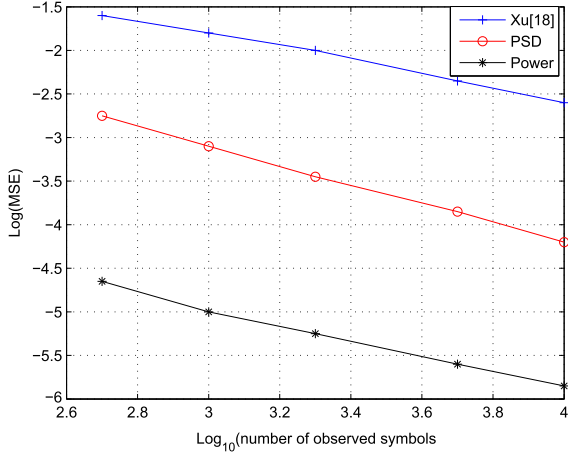
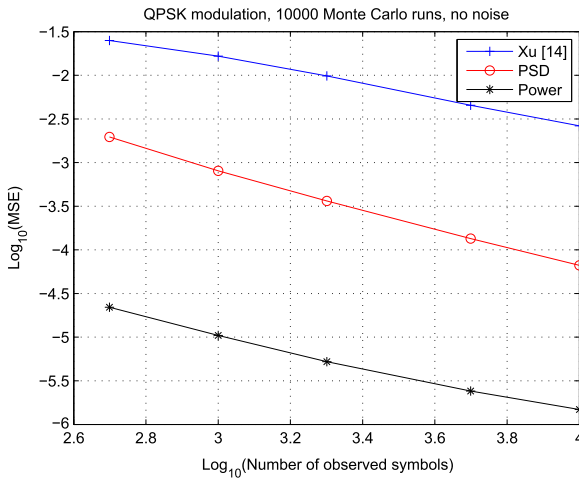
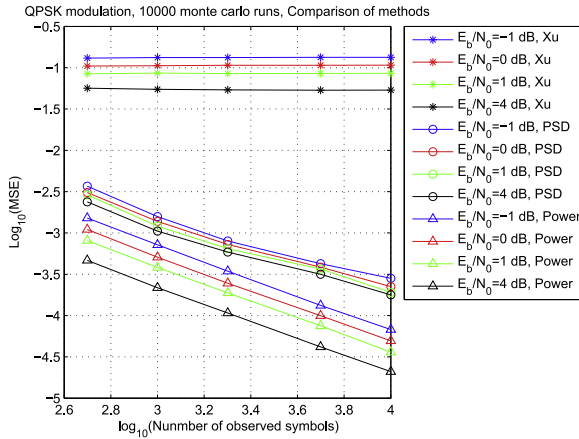
$$\text{SNR}_w = \frac{\sigma_d^2 g^2(t_0)}{2\sigma^2} = \log_2(M) g^2(t_0) \frac{E_b}{N_0} \quad (33)$$

which is an increasing function of M ¹. We will focus on the QPSK modulation in the rest of the paper.

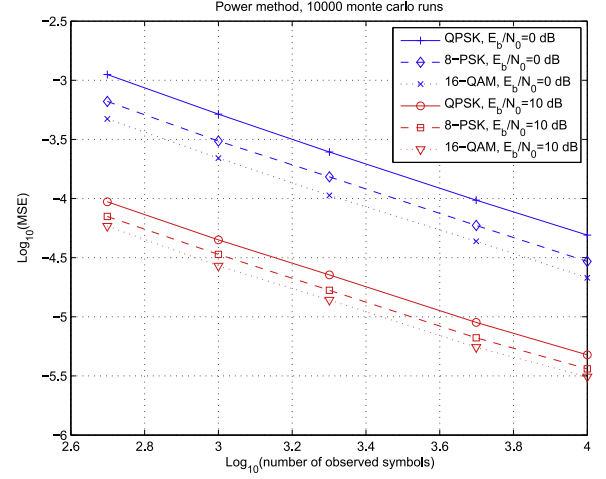
6.3. Estimation errors and MCRBs

This section compares the MSEs of the power based roll-off estimator with the corresponding MCRBs. All simulations are shown for the QPSK modulation and do not change significantly for other modulations. Fig. 12(a) compares the MSEs and MCRBs, as a function of N_s for three values of E_b/N_0 , whereas Fig. 12(b) shows a comparison

¹ Note that it is not necessary to demodulate the signal to estimate the roll-off. Consequently, the performance of the estimation method is not related to E_b/N_0 (like BER) but to the SNR E_s/N_0 , where $E_s = E_b \log_2(M)$.

(a) $E_b/N_0 = \infty$.(b) $E_b/N_0 = 0\text{ dB}$.**Fig. 9.** Estimated logMSEs as a function of the number of observed symbols for a QPSK modulated signal.**Fig. 10.** Estimated logMSEs as a function of the number of observed symbols for several values of E_b/N_0 .

as a function of the emitted roll-off α_e for $N_s=2000$ observed symbols and $E_b/N_0 = 0\text{ dB}$. The obtained MSEs and MCRBs present the same trends and are quite close. Indeed, the average differences between the two curves are 1.40 dB for $E_b/N_0 = 0\text{ dB}$, 0.94 dB for $E_b/N_0 = 5\text{ dB}$ and 0.89 dB for $E_b/N_0 = 10\text{ dB}$.

**Fig. 11.** Power-based estimation method: logMSEs for QPSK, 8-PSK and 16-QAM modulations in the presence of noise.

6.4. Robustness to channel impairments

The transmission channel is affected by several impairments in most practical applications. These impairments include synchronization errors for the carrier phase and frequency. Since the noise is independent from the received data, the theoretical PSD of the received signal (and its integral yielding the power) is insensitive to the presence of a phase shift. More precisely, the PSD of the complex envelope

$$r(t) = \sum_k d_k h(t - kT_s) e^{j\phi} + n(t) \quad (34)$$

does not depend on the phase error ϕ . Thus the presence of a phase shift should not impact either the proposed roll-off estimation methods, or the method studied in [26]. The situation is different when the received signal is affected by a carrier frequency error Δf . In this case, the complex envelope of the received signal can be written

$$r(t) = \sum_k d_k h(t - kT_s) e^{j2\pi\Delta f t} + n(t). \quad (35)$$

The effect of the frequency error is to shift the useful part of the PSD around the frequency Δf inducing a mismatch between $S_r(f)$ and $S(f, \alpha_e)$. Some additional ISI also appears since the transfer function of the emitted filter $H(f)$ is also shifted resulting in a global transmission channel $G(f)$ that does not fulfill the Nyquist criterion. In order to analyze the effect of frequency errors, we have tested the roll-off estimation methods for a QPSK modulation, without noise ($E_b/N_0 = 100\text{ dB}$), for $E_b/N_0 = 0\text{ dB}$ and for different values of the frequency error normalized by the symbol rate, i.e., $\Delta f/R_s$. Figs. 13, 14 and 15 show the precision of the three studied roll-off estimators (square root of the MSE) as a function of $\Delta f/R_s$ for different values of N_s . Note that $\Delta f/R_s$ can reach a value of 25% in a DVB-S2 system, but can be significantly reduced by implementing a correction process such as, for example, a blind carrier frequency offset estimation algorithm [28]. Depending on the desired roll-off estimation precision, Figs. 13, 14 and 15 allow us to determine the appropriate required precision for the carrier frequency error correction process.

6.5. Real data

The proposed power-based estimation method has been finally tested on real signals provided by Thales Alenia Space. In order to test our power roll-off estimation method on real data, two sets of data have been sent on an AWGN channel and recorded by the TCA: BPSK modulated data with roll-off $\alpha_e = 0.35$ and QPSK modulated data with roll-off $\alpha_e = 0.4$. Several values of E_s/N_0 have been considered (5, 10, 15

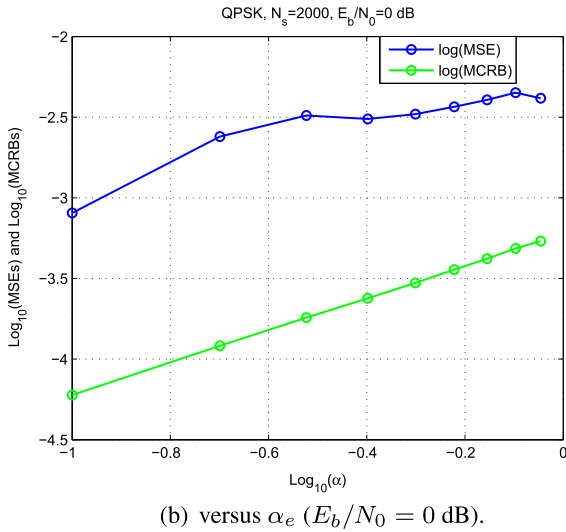
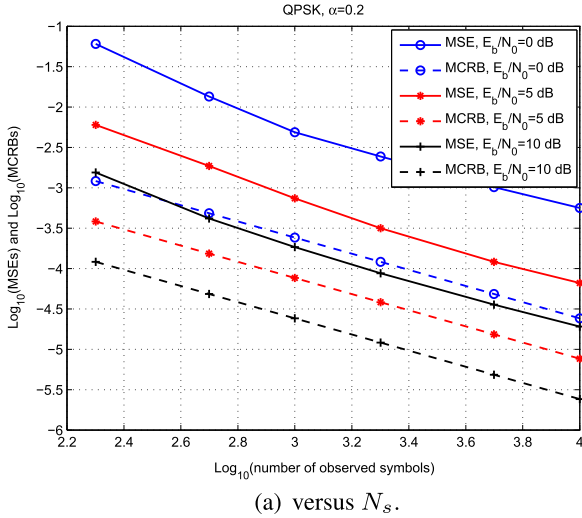


Fig. 12. MSEs and MCRBs for a QPSK modulation and the power-based estimation method.

and 20 dB). The baseband in-phase and quadrature recorded components sampled at $2 R_s$ were used for roll-off estimation. The sampling frequency, the center frequency and the bandwidth were adjusted to

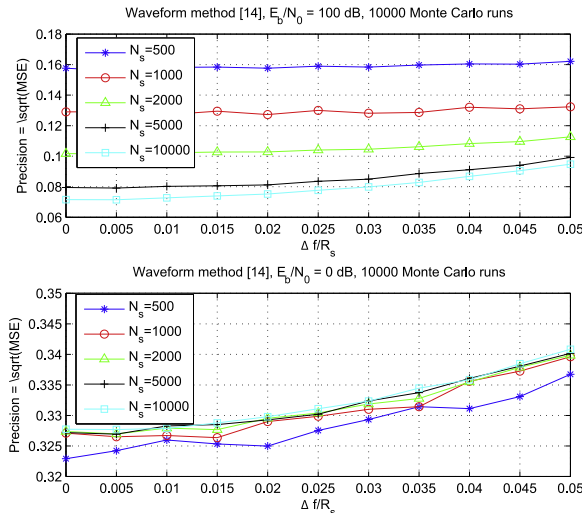


Fig. 13. Squared root MSE of the Xu based roll-off estimator [26] in the presence of a carrier frequency error.

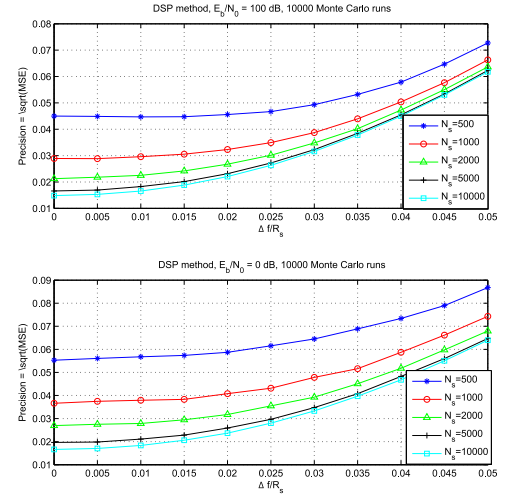


Fig. 14. Squared root MSE of the PSD-based roll-off estimator in the presence of a carrier frequency error.

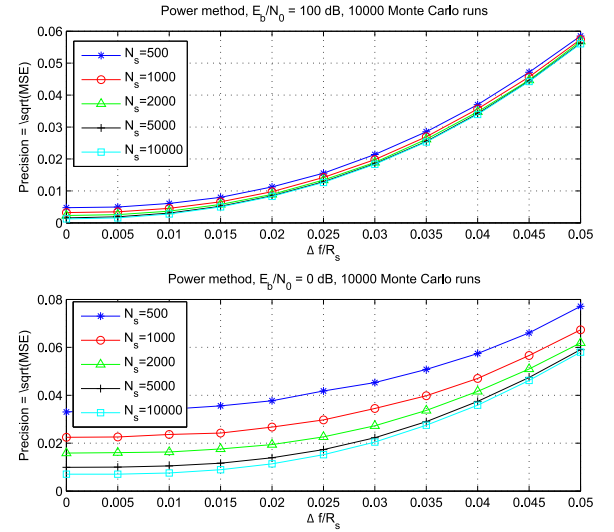


Fig. 15. Squared root MSE of the power-based roll-off estimator in the presence of a carrier frequency error.

11.71875 MHz, 3890 MHz and 5859.375 kHz. Each baseband signal was then divided into 100 blocks of 10000 symbols and the roll-off was estimated for each block. The obtained results are given in Tables 3, 4. The means, variances and MSEs were computed from 100 blocks for each value of E_s/N_0 . The results are coherent with the ones obtained with the synthetic data. As expected, the precision increases with SNR, and with the modulation order for a given E_b/N_0 (e.g., compare estimates resulting from a BPSK constellation with $E_s/N_0 = E_b/N_0 = 5$ dB given in the first line of Table 3 with estimates resulting from a QPSK constellation with $E_s/N_0 = 2E_b/N_0 = 10$ dB given in the second line of Table 4).

7. Conclusions

In order to perform digital modulation classification, the receiver has to know or to estimate some key parameters associated with the transmitted communication signal. This paper addressed the problem of estimating the roll-off factor of a classical square root raised cosine shaping filter. We first analyzed the impact of a roll-off mismatch on the bit error rate (directly related to the modulation classifier performance). Then, we proposed two roll-off estimation methods and compared them to a benchmark available in the literature [26]. The two proposed methods are based on the power spectral density and on

Table 3BPSK modulated signal, $\alpha_e = 0.35$.

E_s/N_0	Mean	Variance	$\log_{10}(\text{MSE})$	Precision
5 dB	0.3340	$2.9309 \cdot 10^{-4}$	-3.2604	0.0234
10 dB	0.3338	$5.4552 \cdot 10^{-5}$	-3.4990	0.0178
15 dB	0.3351	$2.2757 \cdot 10^{-5}$	-3.6112	0.0156
20 dB	0.3349	$6.9306 \cdot 10^{-6}$	-3.6290	0.0153

Table 4QPSK modulated signal, $\alpha_e = 0.4$.

E_s/N_0	Mean	Variance	$\log_{10}(\text{MSE})$	Precision
5 dB	0.419	$2.3299 \cdot 10^{-4}$	-3.2262	0.0244
10 dB	0.4179	$7.577 \cdot 10^{-5}$	-3.4021	0.0199
15 dB	0.4154	$1.8353 \cdot 10^{-5}$	-3.5926	0.0160
20 dB	0.4162	$7.8 \cdot 10^{-6}$	-3.5683	0.0164

the power of the received signal. The performance of these two methods have been analyzed and their robustness to channel impairments (including white Gaussian noise and synchronization errors) has been studied. Several experiments have shown the good performance of the power-based estimation method. The modified Cramer–Rao bound [7] for the roll-off estimation problem was also derived and compared to the obtained MSEs. Simulations performed on real satellite signal measurements (provided by Thales Alenia Space) finally showed the applicability of the proposed methods to real systems such as the telecom carrier analyzer of Thales Alenia Space. Future work include the performance analysis of modulation classifiers when the roll-off has been estimated with the proposed algorithm.

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